

April 6, 2017 to April 11, 2017 Pond 4 Discharge Calculations

Atlantic Richfield Company's (AR) Leviathan Pond 4 Volumetrics October 2011 spreadsheet was used to calculate the following Pond 4 discharge volumes.

On April 6, 2017 when RWQCB personnel first discovered the partially detached overflow pipe, the reading on the USGS staff gauge that was attached to the overflow pipe (and has since been replaced) was approximately 6.6 ft (see attached photo). The base of the partially detached overflow pipe is at approximately 5.5 ft according to the USGS staff gauge. The corresponding elevation for the staff gauge reading of 6.6 ft and 5.5 ft on AR's Volumetrics spreadsheet (see attached spreadsheet) would be an elevation of 6914.1 and 6913.0 respectively. In determining the discharge volume, it is assumed AR used a USGS staff gauge elevation of 6.5 ft which is an elevation of 6914.0 on AR's Volumetrics spreadsheet.

According to AR's Volumetrics Spreadsheet:

The volume of water located in Pond 4 at an elevation of 6914.1 is 3909 yd³

The volume of water located in Pond 4 at an elevation of 6914.0 is 3801 yd³

The volume of water located in Pond 4 at an elevation of 6913.0 is 2767 yd³

From the night of April 6, 2017 till April 11, 2017, when final repair of the Pond 4 overflow was completed, approximately three inches of total moisture fell at the SNOTEL Site located on Monitor Pass. According to USGS staff readings, the upper Pond elevations increased by 0.2 ft during this time period due to direct precipitation. Since the upper Pond elevations are a more accurate representation of site conditions, the 0.2 ft is used in the calculations that include direct precipitation. According to AR's Pond 4 survey data from 2012, the surface area on which direct precipitation runs into Pond 4 is approximately 36,400 ft². Given the surface area of 36,400 ft² and a direct precipitation amount of 0.2 ft, approximately 7280 ft³ or 270 yd³ of direct precipitation entered Pond 4 between April 6, 2017 and April 11, 2017.

The temporary repair performed by AR on April 7, 2017 was successful at reducing Pond 4 discharge flow to Leviathan Creek for only a short period of time. At 15:42 on April 7, 2017, RWQCB personnel observed that the temporary repair of the Pond 4 overflow pipe had failed. From April 7, 2017 till the final repair on April 11, 2017 Pond 4 discharged to Leviathan Creek until Pond 4 reached the USGS staff gauge reading of 5.5 ft. This would result in the elevation of Pond 4 being 6913.0 on April 11, 2017 when the Pond 4 overflow was repaired.

Given the above information, the following discharge amount scenarios have been calculated:

1 foot of discharge from Pond 4 not including direct precipitation

$$3801 \text{ yd}^3 - 2767 \text{ yd}^3 = 1034 \text{ yd}^3 \text{ (208,837 gallons)}$$

1.1 feet of discharge from Pond 4 not including direct precipitation

$$3909 \text{ yd}^3 - 2767 \text{ yd}^3 = 1142 \text{ yd}^3 \text{ (230,650 gallons)}$$

1 foot of discharge from Pond 4 including direct precipitation

$$3801 \text{ yd}^3 - 2767 \text{ yd}^3 + 270 \text{ yd}^3 = 1304 \text{ yd}^3 \text{ (263,374 gallons)}$$

1.1 feet of discharge from Pond 4 including direct precipitation

$$3909 \text{ yd}^3 - 2767 \text{ yd}^3 + 270 \text{ yd}^3 = 1412 \text{ yd}^3 \text{ (285,187 gallons)}$$

Since the Mine site did receive precipitation from April 6, 2017 to April 11, 2017, one of the last two discharge amount scenarios would be the most plausible.



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Leviathan Pond 4 Volumetrics October 2011

Outlet elevation 6916.03, Transducer elevation 6910.49

Elevation	Volume in interval (cu yds)	Volume below elevation (cu yds)	Area at elevation (sq ft)	
6909.1		0	8	
	0			
6909.2		0	37	
	2			
6909.3		2	1442	
	10			
6909.4		12	4134	
	21			
6909.5		33	6896	
	30			
6909.6		63	9418	
	40			
6909.7		103	11922	
	48			
6909.8		151	13766	
	54			
6909.9		205	15342	
	60			
6910.0		265	16819	
	64			
6910.1		329	17858	
	68			
6910.2		397	18510	
	70			
6910.3		467	18988	
	71			
6910.4		538	19423	Assumed water depth at shutdown
	73			Volume
6910.5		611	19831	108654.5 Gal
	74			
6910.6		685	20207	
	75			
6910.7		760	20514	
	77			
6910.8		837	20790	
	78			
6910.9		915	21062	
	79			
6911.0		994	21334	
	80			
6911.1		1074	21593	
	81			
6911.2		1155	21852	
	82			
6911.3		1237	22111	

	82		
6911.4		1319	22371
	83		
6911.5		1402	22632
	84		
6911.6		1486	22893
	85		
6911.7		1571	23150
	86		
6911.8		1657	23405
	87		
6911.9		1744	23661
	88		
6912.0		1832	23917
	89		
6912.1		1921	24170
	90		
6912.2		2011	24425
	91		
6912.3		2102	24680
	92		
6912.4		2194	24937
	93		
6912.5		2287	25196
	94		
6912.6		2381	25455
	95		
6912.7		2476	25716
	96		
6912.8		2572	25978
	97		
6912.9		2669	26241
	98		
6913.0		2767	26501
	99		
6913.1		2866	26760
	100		
6913.2		2966	27022
	101		
6913.3		3067	27285
	102		
6913.4		3169	27550
	103		
6913.5		3272	27815
	104		
6913.6		3376	28078
	105		
6913.7		3481	28335
	106		
6913.8		3587	28586
	107		
6913.9		3694	28837

	107				
6914.0		3801	29086		
	108				
6914.1		3909	29330		
	109				
6914.2		4018	29574		
	110				
6914.3		4128	29816		
	111				
6914.4		4239	30058		
	112				
6914.5		4351	30301		
	113				
6914.6		4464	30545		
	114				
6914.7		4578	30790		
	115				
6914.8		4693	31036		
	116				
6914.9		4809	31284		
	117				
6915.0		4926	31533	Assumed Max Capacity (1 foot below outlet elevation)	
	117			Additional 0.03 feet	
6915.1		5043	31783	Volume	Surface Area
	118			35.1	74.976
6915.2		5161	32034	Gal	Feet
	119				
6915.3		5280	32286		
	120				
6915.4		5400	32540		
	121				
6915.5		5521	32794		
	122				
6915.6		5643	33050		
	123				
6915.7		5766	33307		
	124				
6915.8		5890	33566		
	125				
6915.9		6015	33825		
	126				
6916.0		6141	34086	Outlet	
	118			Additional 0.03 feet	
6916.1		6259	34351	Volume	Surface Area
				35.4	79.677
				Gal	Feet